

# Retrofitting an existing heating system with a heat pump.

Gert Nielsen  
Managing Geek  
Xrgy AS  
gert.nielsen@xrgy.no

# What are we looking at today

- We will be looking at retrofitting an older building, designed according to the Norwegian BF1987<sup>1</sup>, but located in London, with a heat pump system.
- Year of build 1990. (Make believe)
- We will look into what data you will have to gather, how to acquire these data.

BF = Byggeforskrift = Building Code

# What are we looking at today

- Cosmetic changes on the inside might occur.
- Carpets will be replaced with laminate. (Much better for indoor climate)
- If at all possible the pipework for radiators, heating and cooling coils will be kept.
- New air handling units will be installed. At an age of 30+ years their technical life has expired.

# Most buildings have already been built.

- When retrofitting an existing building to accommodate a heat pump, you have to know / find out the following:
- Design conditions for the building
  - Design ambient temperature.
  - Design temperatures in the radiator system.
  - Design heat delivery from the radiator system.
  - Design temperatures in the ventilation heating system.
  - Design air flow for the ventilation heating system. Not necessarily the same as the total design air flow.
  - Recuperator efficiency.
  - Fan power demand in the AHUs, especially on the incoming air.

# Most buildings have already been built.

- In short, all the design parameters that affect the thermal performance of the building, and hopefully taken into consideration originally.
- You would think this information is readily available from when the building was built.

**HA!! Think again.**

# But first, a trip to Oslo

- A client needed to replace a run down chiller.
- 4 circuit R22 unit, 2 circuit didn't work.
- My colleague on site (a man with 50 years of experience) suggested a reversible unit.
- Supplying ventilation heat during winter.
- Why not use it to supply building heat as well?
- Problems or more PC :
- Challenges

# Documentation

- The building owner is basically only interested in money.
- The level of documentation of the systems are fundamentally non-existent.
- Historical energy demands exist only as invoices in NOK.
- The old oil boiler had been converted to electrical heating. The boiler itself had not been replaced
- No overall control systems, unitary control of the individual subsystems.

# Documentation

- The only documentation was a ventilation service report from 2012.
- Riddled with errors.
- The heating coil was not able to supply enough heat to reach set point temperature, so to electrical heating coils had been added in the duct system.
- The service contractor had missed this, and believed that the coil recuperator system was hugely efficient at 45%.
- Our combined experience of 80 years said “No effing way”
- Taking into account the total electrical coil performance, the efficiency ended up at 27% which fits our experience.

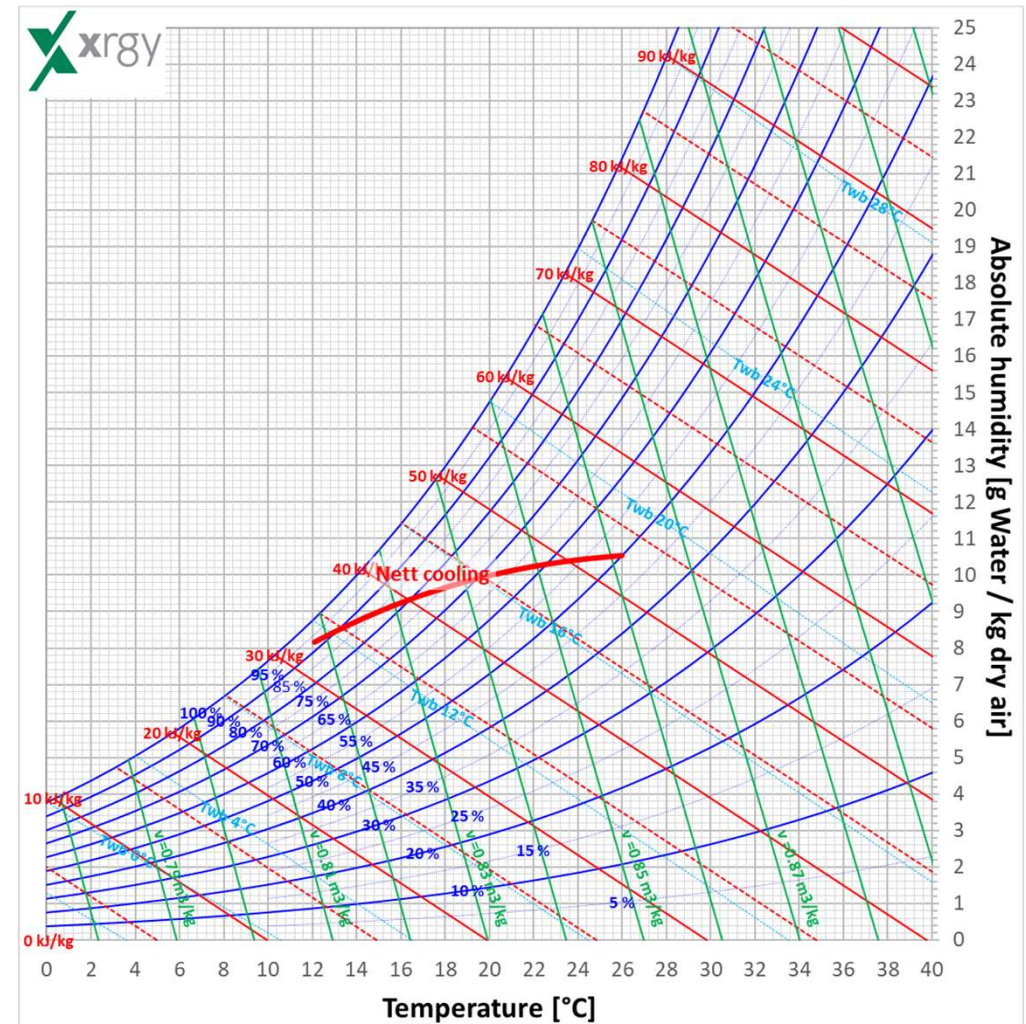


# Documentation

- Summer    Airflow supply    15 000 m<sup>3</sup>/h    Fan power    14 kW
- Winter    Airflow supply    9 570 m<sup>3</sup>/h    Fan power    3,6 kW
- The winter air flow and fan power is assessed from the model laws.
- Temperature rise from fan power
  - Summer    2,8K
  - Winter    0,7K
- Cold demand is design performance for the heat pump.
- The existing chiller was designed for 100 kW at 7°C/12°C.
- The inlet temperature should be app. 15°C to remove internal heat loads.

# Cold demand

- Parasitical load from fan power is app. 23% of the cold demand.
- New requirements for fan power reduces the cold demand significantly



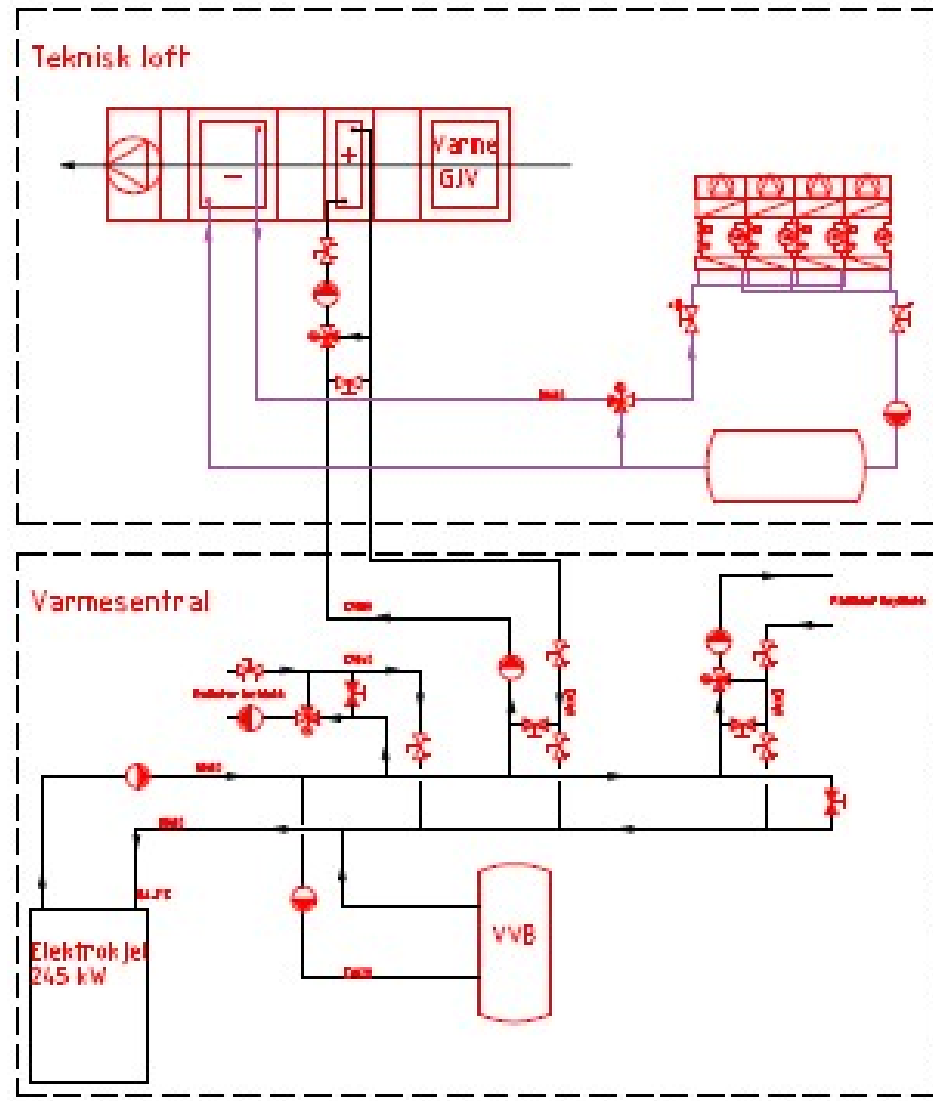
# Heat demand

- All of these are assessments based on building area and experience.
- Heat demand building heating      105 kW
- Heat demand ventilation heating      100 kW

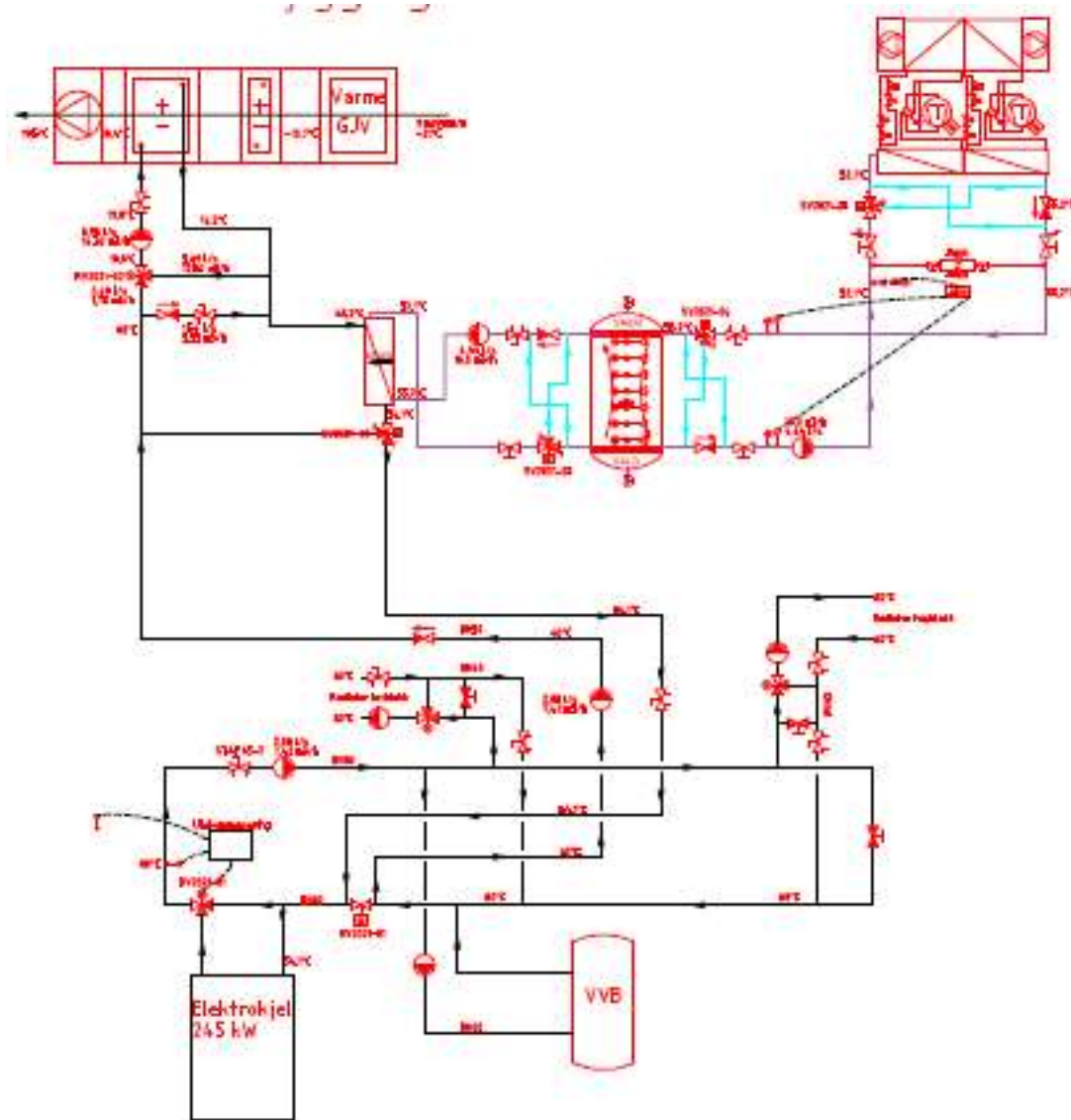
# Structural issues

- Air handling unit and chiller are located on the roof
- Boiler and headers are located in the basement, 3 storeys below the roof.
- In the system as it is today, there is no connection between the chiller and the heating system.

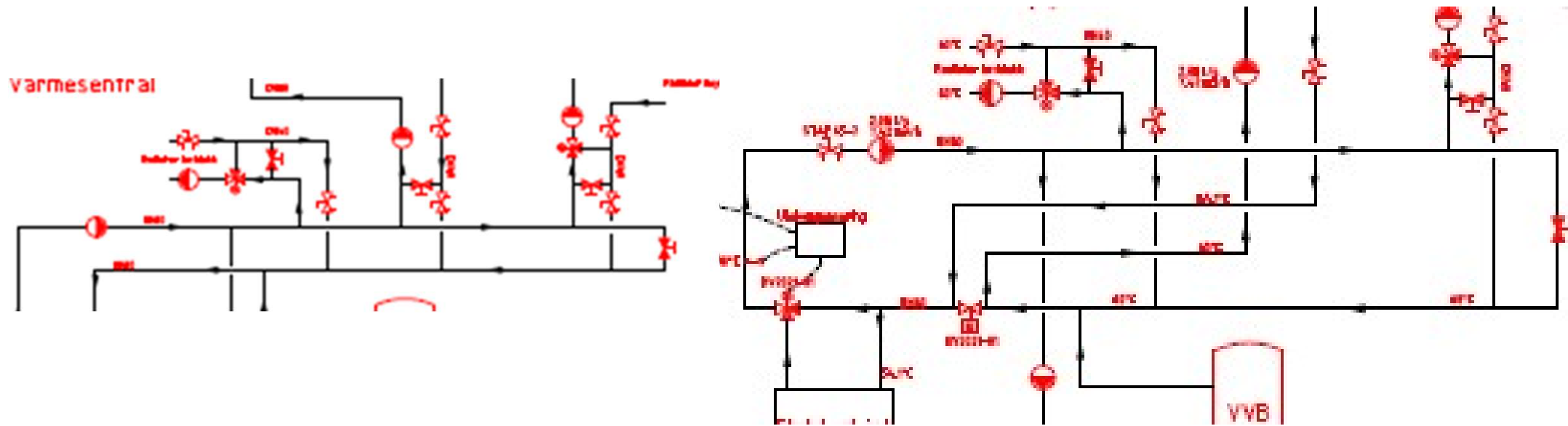
# Situation today



# New system



# New system



# Changes from today to planned system

- The cooling coil now works as a combicoil
- The header connection to ventilation heating is in series with the building heating strings.
- The heating system gets heat from the heat pump before being heated from the boiler.
- The controls are expanded to handle the entire building in a top system.



# Basically we knew nothing

- This project is a very good example of why experience is important.
- We will know take a 10 minute break, and return to London.

# Data acquisition

- Knowing what demands you need to cover NOW is crucial.
- Old Building Management Systems are usually only good at telling if someone has stolen the equipment.
- The following statement started as a provocation, but turns out to be largely true :
- **"The intelligence of the Building Management System will over time drop to reach the level of the building operators"**
- The fault here is largely management.
- Management will usually not give priority to keeping the operators educated and well trained

# Typical organisational problems

- Buildings are usually managed by accountants.
- Goal is to maximise profits
- => reduce cost.
- Maintenance
- Avoid maintenance.
- Education of operators
- I am not going to pay for others getting better operators!!

# Typical organisational problems

- Avoid education of operators.
- Result : Reduced quality over time.
- Result of that: Tenants leaving.
- To keep the building occupied and some money coming in =>
- Rent reduction => decrease in profits
  
- Downward spiral of cost cutting, quality reduction, reduced rent.
  
- And the poor sod in charge doesn't understand what is going on.

# Typical organisational problems

- What we must teach the building managers :
- Maintenance
- Good and proper maintenance maintains the quality of the building.
- Good and proper maintenance avoids downtime and repairs
- Repairs
- Good quality = higher rent.
- Education of operators
- Education of operators :
- Upward spiral of profitability and an easier job!
- Making more money while working less, and having more fun at work!!

# Typical organisational problems

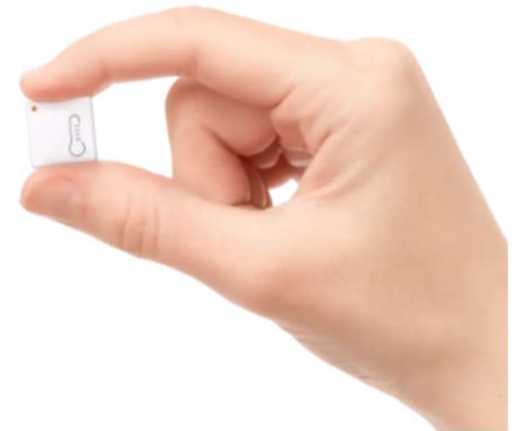
- Engineers and technicians have to learn to speak economy.
- We might have the ideas and the know-how.
- But it is the economy that decides if it will be done.
  
- Don't talk in kWh, kW or similar
- Talk in money and MAYBE in CO<sub>2</sub>-equivalents.
  
- But to convert kWhs and kW into money, we have to establish some basics that we can work from

# Data acquisition

- Typically
  - The points of measurement are too few.
  - The time steps of measurement logging are too long. Normally due to very limited memory capacity on the computers handling the BMS.
- At this time in the life of a building, especially before a major technical overhaul, installing new measurement equipment might be difficult.
- All is not lost...

# Data acquisition

- Small Wi-Fi or Bluetooth temperature sensors can be placed everywhere.
  - This picture was taken from the homepage of Disruptive Technologies (<https://www.disruptive-technologies.com/>)
  - 19x19x2 mm
  - Easily installed, even under insulation.
- 
- What we need most is the energy leaving the machinery room.
  - In old systems like this, it is usually constant flow headers. We therefore only need to know the  $\Delta T$ .





# Data acquisition

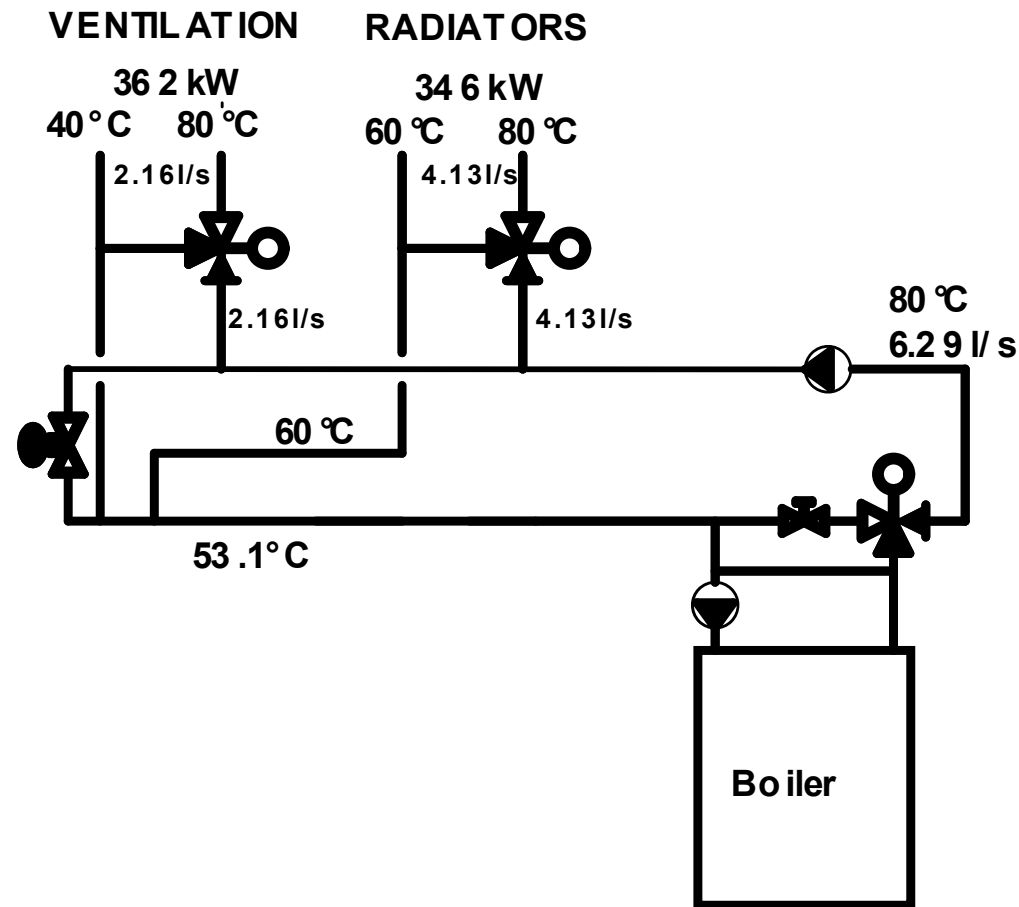
- We also need to know the design winter ventilation rate.
- In systems this old, there will typically only be 50% / 100% flow rates.
- But what is the design performance of the heating coils?
- In my experience they are designed for full flow, even though winter flow is half.
- From that, we end up with

# Baseline assessment

Assesment of heat demand covering transmission and infiltration losses and ventilation heat demand at winter design ventilation rate										
Floor space	17 000 m <sup>2</sup>	Minimum demands from building code		BF1987	Maximum air leakage from building codes		4	Hygienic minimum ventilation rate, building		0 m <sup>3</sup> /h/m <sup>2</sup>
Occupance design	850	U floor		0.3 W/m <sup>2</sup> K	Air change due to infiltration		0.28 per hour	Hygienic minimum ventilation rate, people		21.6 m <sup>3</sup> /h/pers
T soil. Set to annual mean temperature	12 °C	U window		2.4 W/m <sup>2</sup> K	Air flow		14 280 m <sup>3</sup> /h	Total hygienic minimum ventilation rate		1.08 m <sup>3</sup> /h/m <sup>2</sup>
T Indoor	22 °C	U wall		0.3 W/m <sup>2</sup> K	Volume of the building		51 000 m <sup>3</sup>	Actual minimum ventilation rate (9.26)		10 m <sup>3</sup> /h/m <sup>2</sup>
Design Ambient temperature	-4 °C	U roof		0.2 W/m <sup>2</sup> K	Air change		0.280 per hour	Efficiency recuperator in AHU. Highest.		60 %
		leakage number at 50 Pa		4 1/h	Air flow		14 280 m <sup>3</sup> /h	ΔT supply air / room temperature		2 K
		Recuperator efficiency		0 %	Air flow		14 280 m <sup>3</sup> /h	ΔT supply air from fan power		2.1 K
Length of the building	125 m							Your recuperator efficiency demand		60 %
Width	17 m	Transmission			Infiltration			Ventilation		
Number of storeys	8 stk	U floor		0.3 W/m <sup>2</sup> K	Volume of the building		51 000 m <sup>3</sup>	Total air flow		170 000 m <sup>3</sup> /h
Storey hight	3 m	U window		2.4 W/m <sup>2</sup> K	Air change		0.280 per hour	Supply air temperature		20 C
Window share of building envelope	40 %	U wall		0.3 W/m <sup>2</sup> K	Air flow		14 280 m <sup>3</sup> /h	Supply air temperature after recuperator		11.6 C
Incline roof	12 °	U roof		0.2 W/m <sup>2</sup> K				Supply air temperature after heating coil		17.9 C
Roof width	17.38 m	Heat loss floor		6 375 W				ΔT heating coil		6.3 K
Area floor to ground (footprint)	2 125 m <sup>2</sup>	Heat loss windows		170 127 W				Heat demand heating coil		362 355 W
Area building fasades	6 816 m <sup>2</sup>	Heat loss walls		32 138 W				Heat demand from subtemperature supply air		115 033 W
Area windows	2 726 m <sup>2</sup>	Heat loss roof		11 297 W						
Wall area from gable/roof incline	30.7 m <sup>2</sup>	<b>Total transmision heat loss</b>		<b>219 938 W</b>	<b>Q infiltrasjon</b>		<b>125 616 W</b>			
Area wall	4 120 m <sup>2</sup>	<b>Q trans og inf.</b>		<b>345 554 W</b>						
Area roof	2 172 m <sup>2</sup>	<b>Q tot, design building heating</b>		<b>460 587 W</b>						
		<b>Q tot, design, heating system</b>		<b>822 942 W</b>	<b>822.9 kW</b>					
								q trans & in		48.4 W/m <sup>2</sup>
								q vent		28.1 W/m <sup>2</sup>
								q tot des		48.4 W/m <sup>2</sup>

Design demand = 708 kW when built

# Basic system design



Design

# What has happened from building until today?

- Since the building was erected usually some things have changed.
- Example:
- Windows to more energy efficient.
- Matching the demand from TEK07

# Baseline adjustment

Assesment of heat demand covering transmission and infiltration losses and ventilation heat demand at winter design ventilation rate							
Floor space	17 000 m <sup>2</sup>	Minimum demands from building code	BF1987	Maximum air leakage from building codes	4	Hygienic minimum ventilation rate, building	0 m <sup>3</sup> /h/m <sup>2</sup>
Occupance design	850	U floor	0.3 W/m <sup>2</sup> K			Hygienic minimum ventilation rate, people	21.6 m <sup>3</sup> /h/person
T soil. Set to annual mean temperature	12 °C	U window	2.4 W/m <sup>2</sup> K			Total hygienic minimum ventilation rate	1.08 m <sup>3</sup> /h/m <sup>2</sup>
T Indoor	22 °C	U wall	0.3 W/m <sup>2</sup> K	Air change due to infiltration	0.28 per hour	Actual minimum ventilation rate (9.26)	10 m <sup>3</sup> /h/m <sup>2</sup>
Design Ambient temperature	-4 °C	U roof	0.2 W/m <sup>2</sup> K			Efficiency recuperator in AHU. Highest	60 %
		leakage number at 50 Pa	4 1/h			ΔT supply air / room temperature	2 K
		Recuperator efficiency	0 %			ΔT supply air from fan power	2.1 K
Length of the building	125 m					Your recuperator efficiency demand	60 %
Width	17 m	Transmission		Infiltration		Ventilation	
Number of storeys	8 stk	U floor	0.3 W/m <sup>2</sup> K	Volume of the building	51 000 m <sup>3</sup>	Total air flow	170 000 m <sup>3</sup> /h
Storey height	3 m	U window	1.2 W/m <sup>2</sup> K	Air change	0.280 per hour	Supply air temperature	20 C
Window share of building envelope	40 %	U wall	0.3 W/m <sup>2</sup> K	Air flow	14 280 m <sup>3</sup> /h	Supply air temperature after recuperator	11.6 C
		U roof	0.2 W/m <sup>2</sup> K			Supply air temperature after heating coil	17.9 C
Incline roof	12 °	Heat loss floor	6 375 W			ΔT heating coil	6.3 K
Roof width	17.38 m	Heat loss windows	85 064 W			Heat demand heating coil	362 355 W
Area floor to ground (footprint)	2 125 m <sup>2</sup>	Heat loss walls	32 138 W			Heat demand from subtemperature supply	115 033 W
Area building fasades	6 816 m <sup>2</sup>	Heat loss roof	11 297 W				
Area windows	2 726 m <sup>2</sup>	Total transmission heat loss	134 874 W	Q infiltrasjon	125 616 W		
Wall area from gable/roof incline	30.7 m <sup>2</sup>	Q trans og inf.	260 490 W			q trans&inf	15.3 W/m <sup>2</sup>
Area wall	4 120 m <sup>2</sup>	Q tot, design building heating	375 524 W			q vent	28.1 W/m <sup>2</sup>
Area roof	2 172 m <sup>2</sup>	Q tot, design, building heating system, including	737 879 W		737.9 kW	q tot des	43.4 W/m <sup>2</sup>

New demand = 623 kW with new windows

# What has happened from building until today?

- Since the building was erected usually some things have changed.
- Windows to more energy efficient.
- Matching the demand from TEK07.
- The heat demand of the building envelope is reduced by 86 kW or 25%.
- What will that mean for the maximum supply temperature to the radiator system?
- 10 minutes.

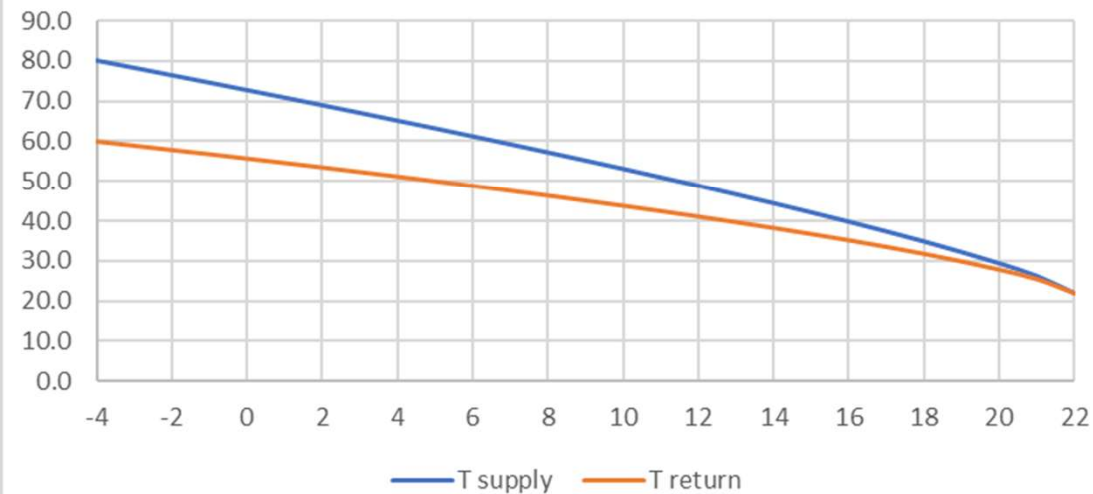


# New temperature demand radiators

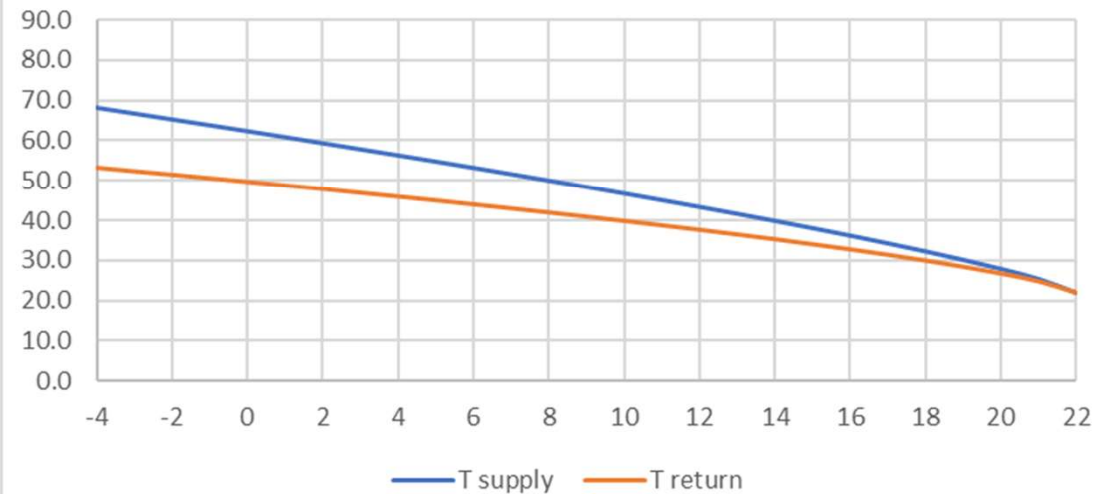
- $\Delta T_{M,RAD,ACT} = \left(\frac{\dot{Q}_{RAD,ACT}}{\dot{Q}_{RAD,DES}}\right)^{\frac{1}{1,3}} \times \Delta T_{M,RAD,DES}; \Delta T_{M,RAD} = \frac{T_{SUPPLY} + T_{RETU}}{2} - T_{ROO}$
- $\Delta T_{M,RAD,DES} = \frac{80+}{2} - 22 = 48K$
- $\Delta T_{M,RAD,ACT} = \left(\frac{260}{346}\right)^{\frac{1}{1,3}} \times 48 = 38.6K \Rightarrow T_{M,RAD,ACT} = 38.6 + 22 = 60.6^{\circ}C$
- $\Delta T_{RAD,ACT} = \left(\frac{260}{346}\right) \times 20 = 15.1K \Rightarrow$
- $T_{SUPPLY,RAD,ACT} = 60.6 + \frac{15.1}{2} = 68.2^{\circ}C$
- $T_{RETURN,RAD,ACT} = 68.2 - 15.1 = 53.1^{\circ}C$

# New temperature demand radiators

Temperature demand in radiatorsystem vs. ambient.



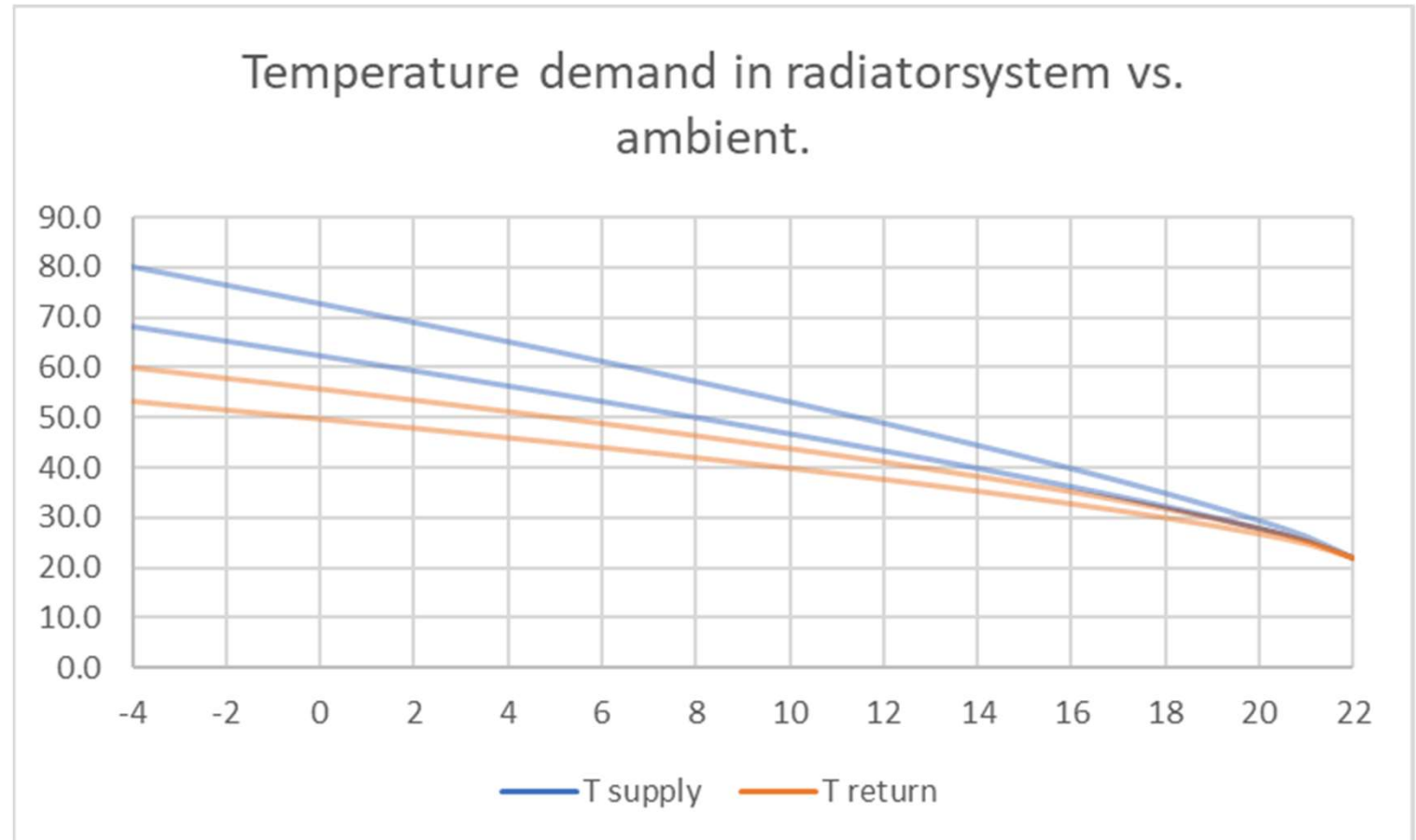
Temperature demand in radiatorsystem vs. ambient.





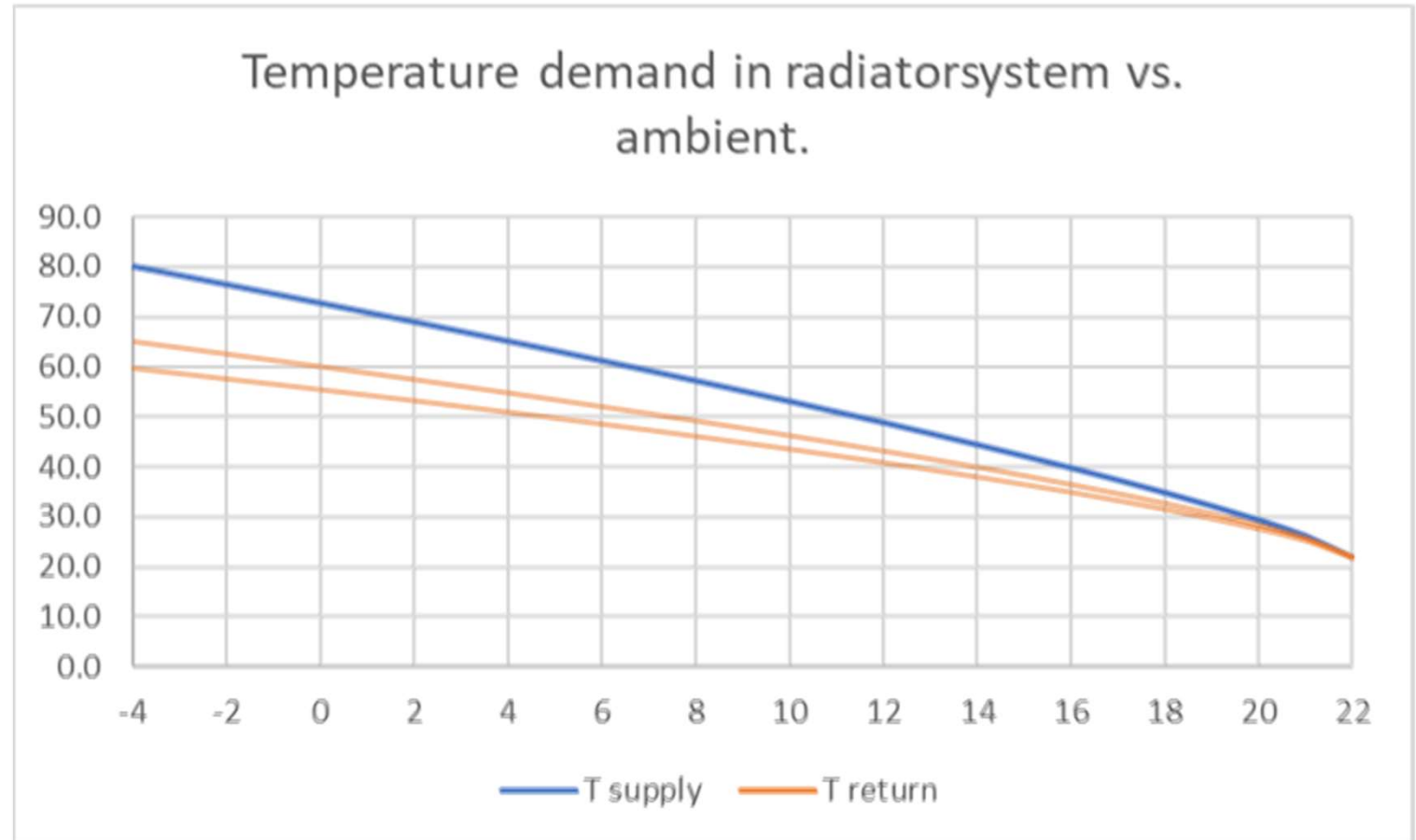
# New temperature demand radiators

- As we see, there is a significant drop in the radiator temperature demand.



# New temperature demand radiators

The result:  
Increase in  
return  
temperature

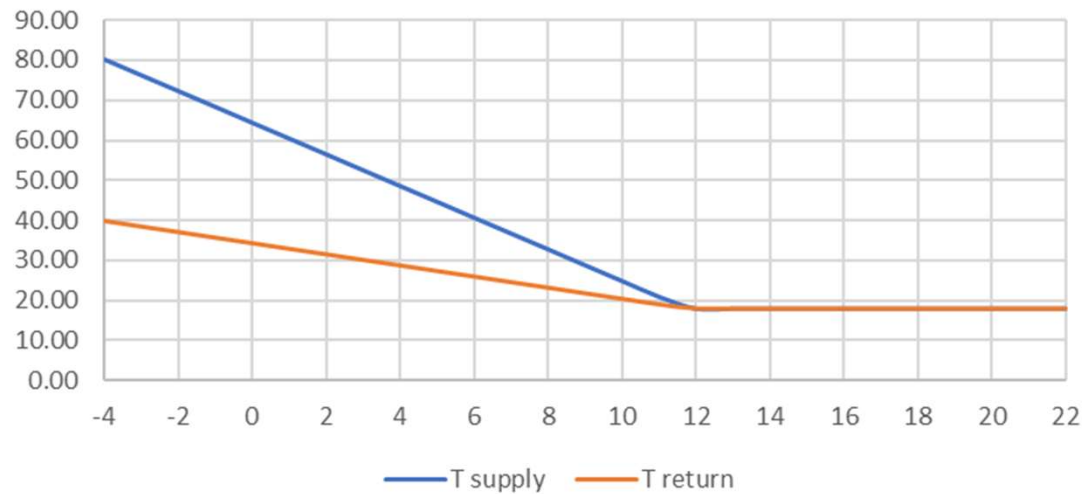


# Actual heat and temperature demand ventilation heating

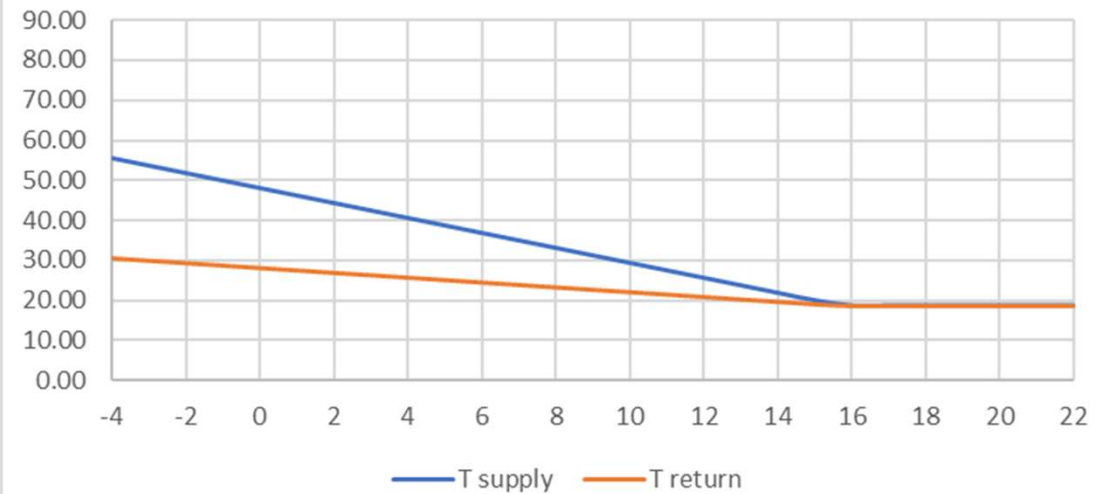
- Heating coil is designed for full flow, 170 000 m<sup>3</sup>/h at -4°C ambient, recuperator temperature efficiency 60%, supply temperature into rooms 20°C, temperature lift from fans 2.1K.
- Heat demand : 362.5 kW.
- Temperature pair heat bearer : 80°C/40°C
- Actual max flow winter is 50% : 85 000 m<sup>3</sup>/h.
- At actual winter flow the temperature lift is therefore 0.53K.
- Heat demand : 226.5 kW

# New temperature demand for heating coil

Temperature demand in heating coil at full flow vs. ambient.



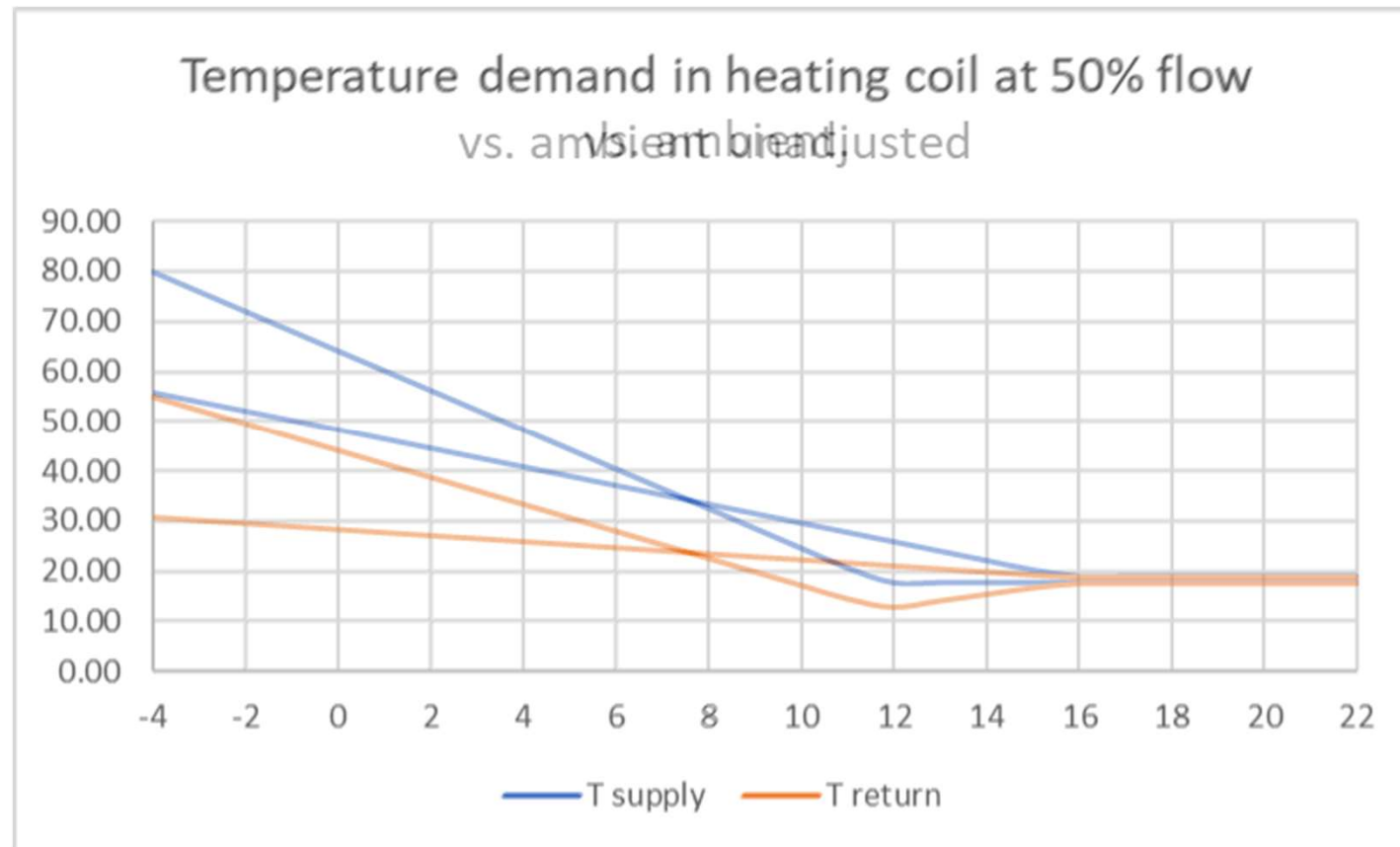
Temperature demand in heating coil at 50% flow vs. ambient.



# New temperature demand for heating coil

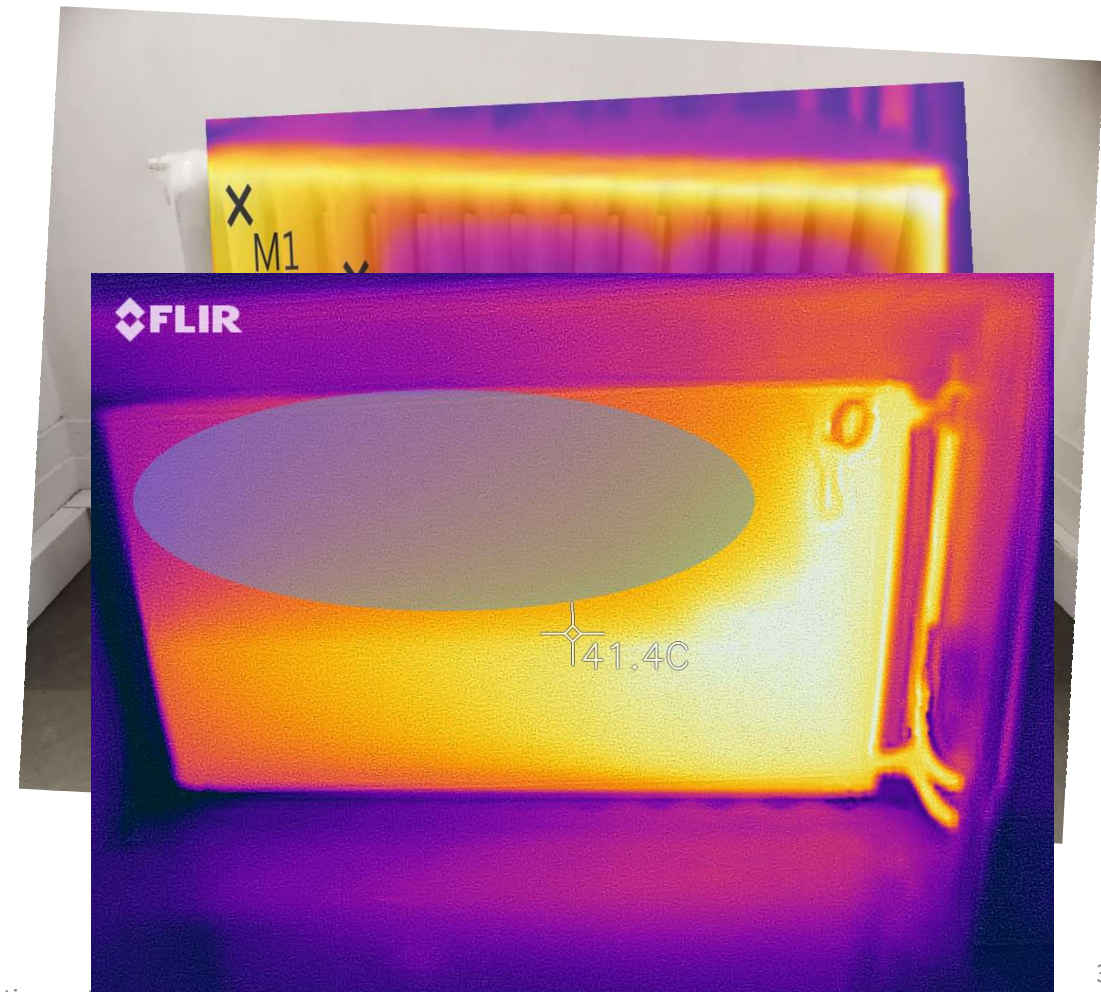
Nobody adjusted the settings

The return temperature is now as high as the supply temperature should have been at design conditions.

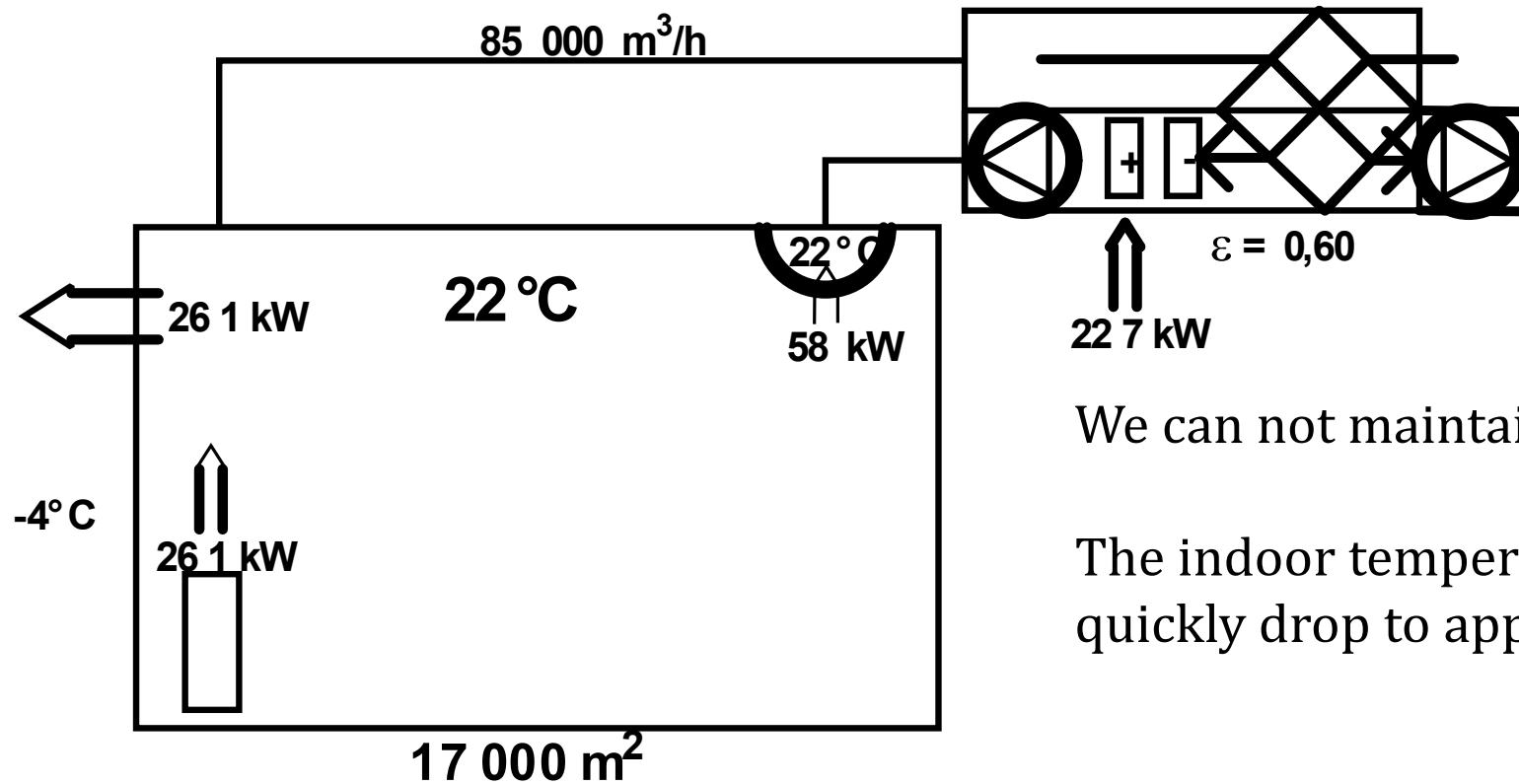


# What has happened from building until today?

- Decay in efficiency of radiators.
- Poor control of water quality, sedimentation
- Air in radiators
- Large air pocket
- Leads to poor performance and higher temperature demand.
- This has to be addressed as well in the new design



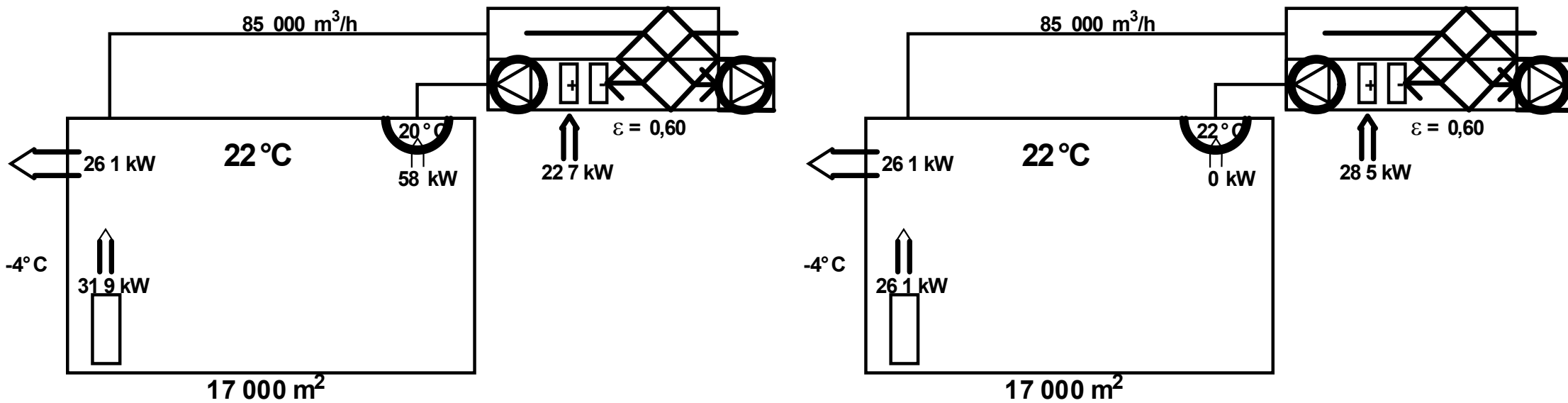
# What happens indoor now?



We can not maintain 22°C.

The indoor temperature will quickly drop to app. 20°C.

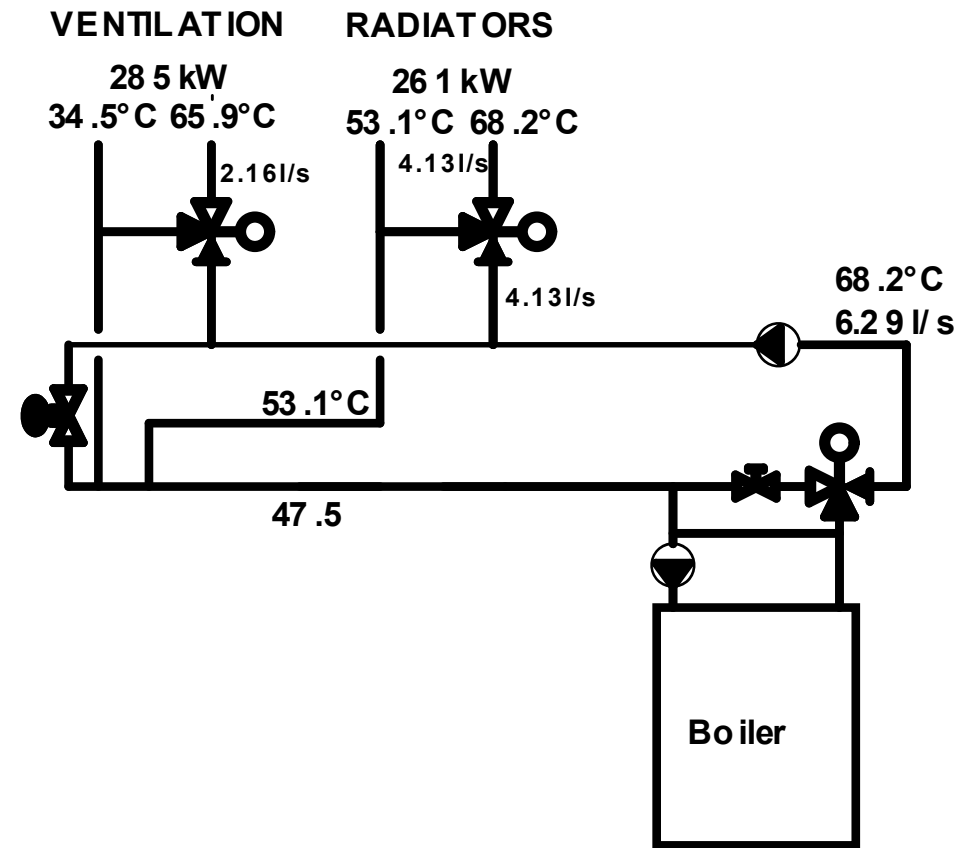
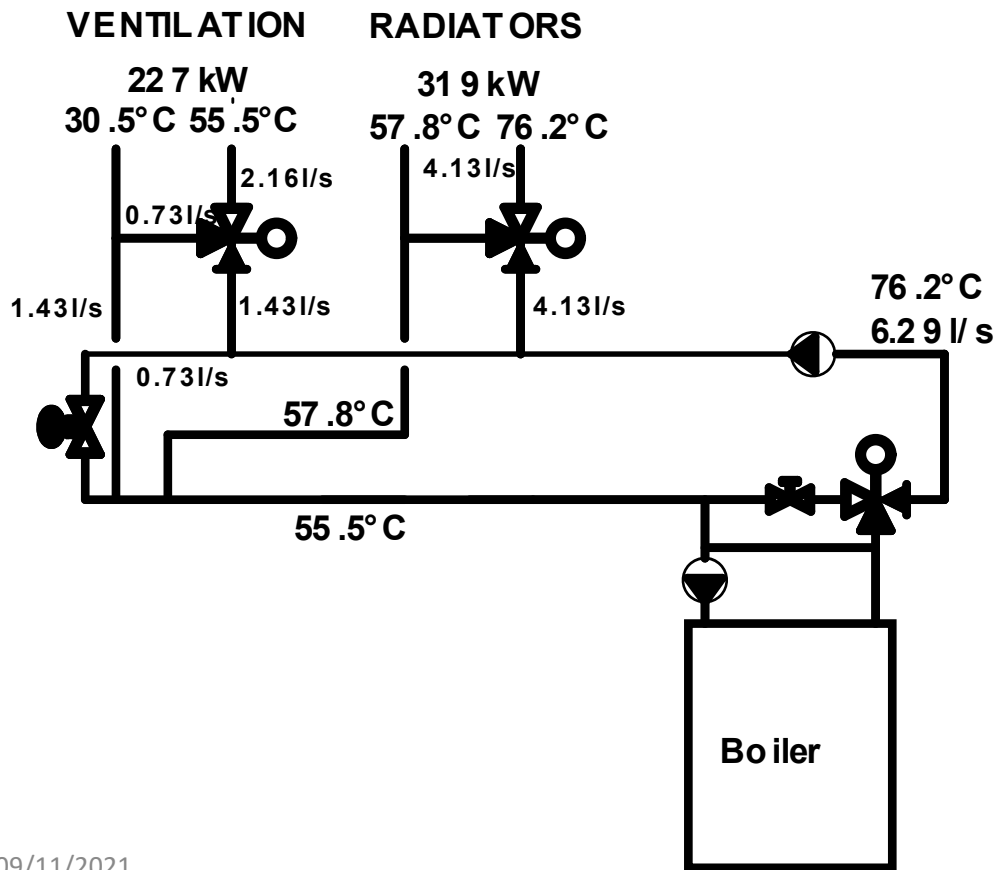
# What happens indoors now?



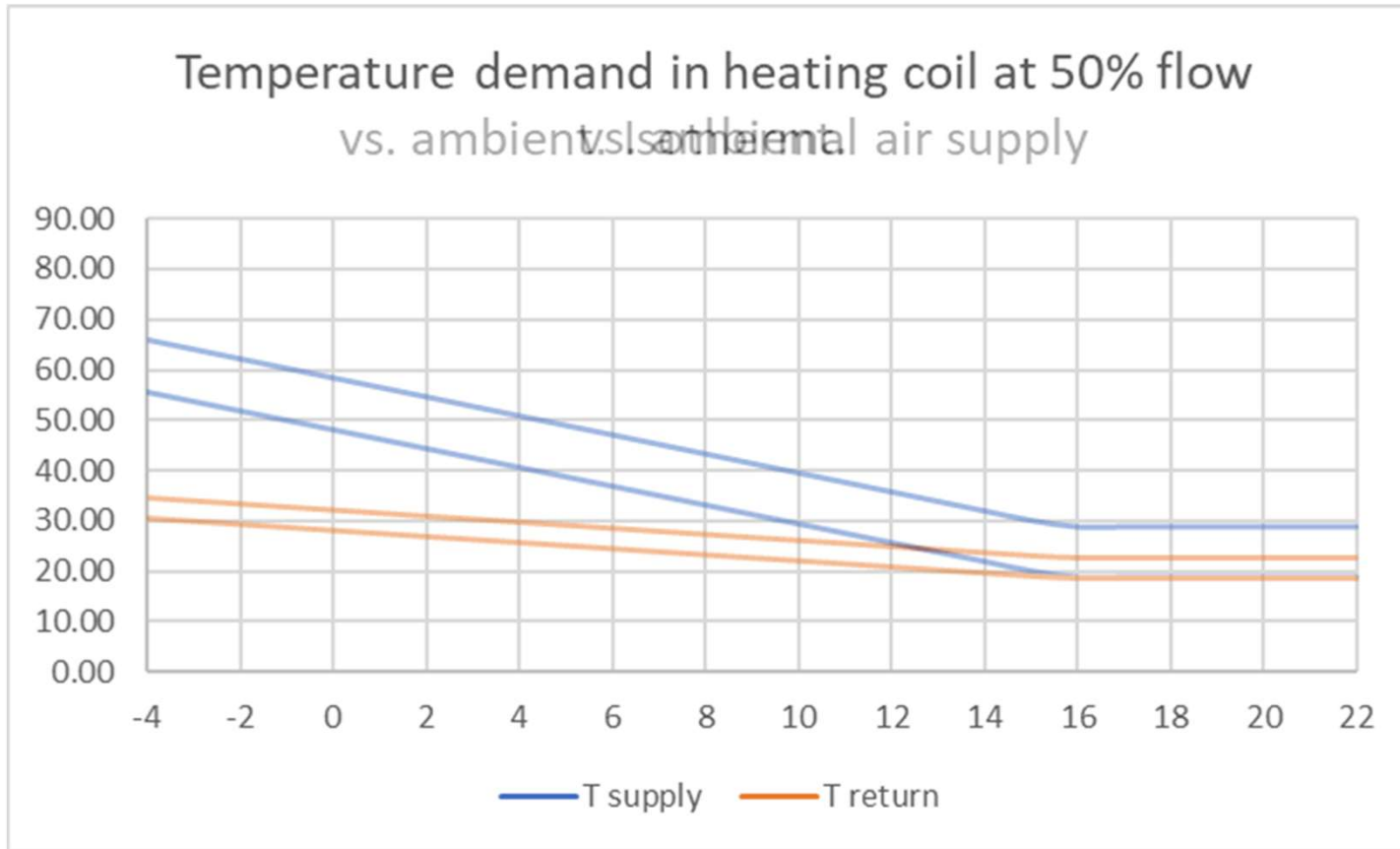
Should we increase the load on the radiators or the heating coils to compensate the 58 kW?  
10 minutes.



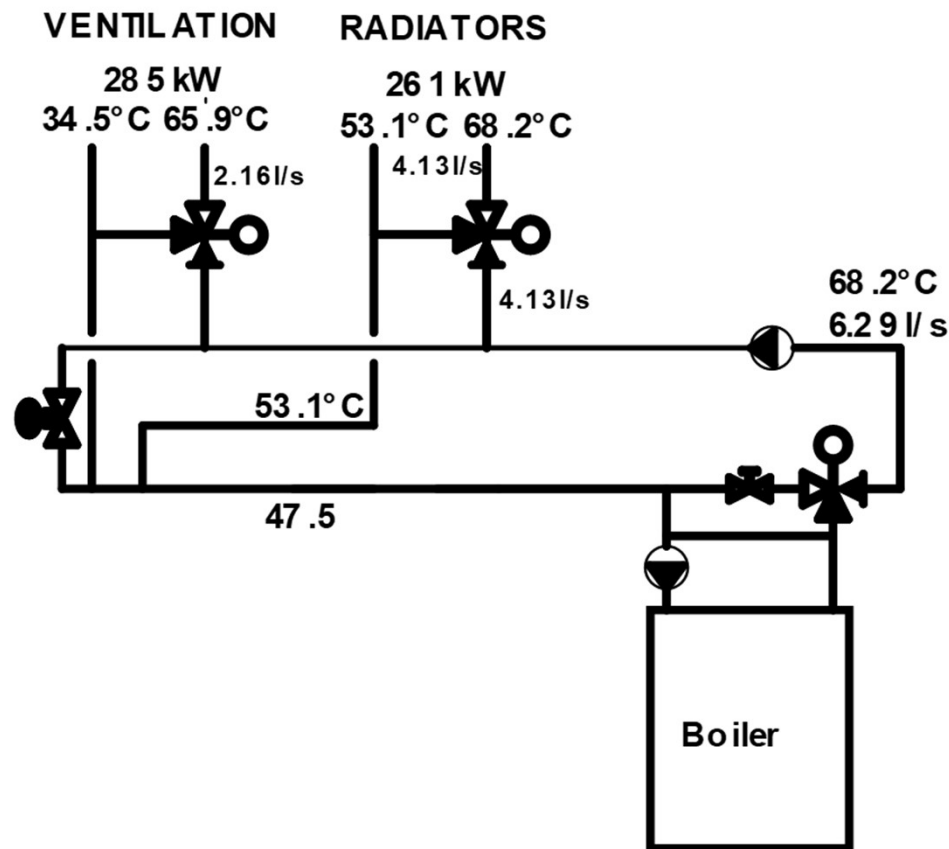
# What to choose? Increase radiator or heating coil load?



# Temperature demand ventilation. Isothermal air supply

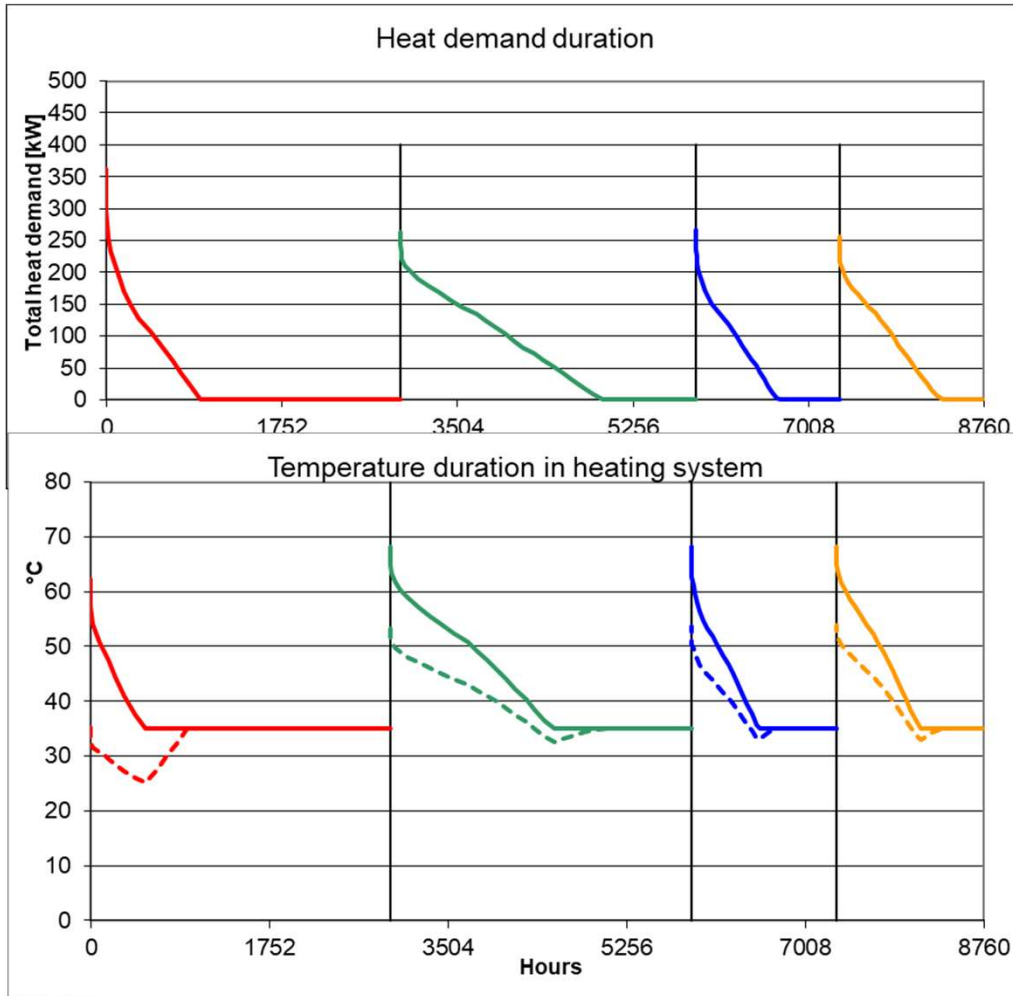


# What happens with the system temperatures?

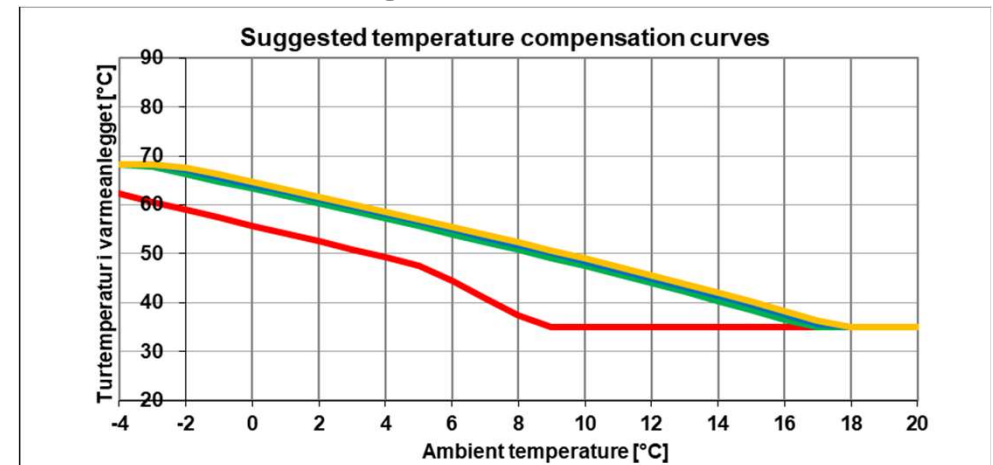


- The maximum design heat demand in the old building, before any retrofitting is 631 kW.
- With new windows it is 545 kW.
- With new windows, lights, computers etc. the annual heat demand is app. 676 MWh.

# System temperature demands



- We want them as low as possible, makes the heat pump run better.
- With the changes already implemented, a heat pump will be able to give a meaningful contribution



# Temperature demand reduction

- In retrofitting an old building with a heat pump, this is the major challenge.
- When changing the AHUs, we have at least two choices.
  - The design flow is found to remove all the internal loads at a  $\Delta T$  of 6K.
  - 850 workspaces, occupancy 80%, each workstation has surplus heat of 100 W from people and 50W from equipment.
  - 17 000 m<sup>2</sup> 5 W/m<sup>2</sup> from lights, 0,5 W/m<sup>2</sup> from misc.
  - Total internal design load : 195,5 kW.
  - Air flow design : 96 300 m<sup>3</sup>/h (5,7 m<sup>3</sup>/h/m<sup>2</sup>).
  - This seems low according to my gut feeling, but I grew up when the lights were 10 W/m<sup>2</sup> and a PC was 150W.

# What if nothing has changed?

- In a professional building you will most likely have a chiller.
- If you have a chiller, you basically have a heat pump.
- If you have cooling of ventilation air, you most likely have a cooling coil.
- The thermal length of a cooling coil is much larger than that of the heating coil.

# Cooling coil as a combi-coil

- The example from the start said
- Heat demand 362 kW.
- Air temperatures                    11.6°C to 17.9°C
- Water temperatures                80°C to 40°C
- $AMTD = (80+40)/2 - (11.6+17.9)/2 = 60 - 14.75 = 45.25 \text{ K}$
- $UA = 362 / 45.25 = 8 \text{ kW/K}$

# Cooling coil as a combi-coil

- Air flow 170 000 m<sup>3</sup>/h
- Ambient 27°C/50%rH
- T of coil 17°C
- Cold bearer 7°C/12°C
- Cold demand 825 kW
- AMTD  $(27+17)/2 - (7+12)/2 = 22-10.5 = 11.5$
- UA  $825 / 11.5 = 71.7 \text{ kW/K}$



# Cooling coil as a combi-coil

- UA  $825 / 11.5 = 71.7 \text{ kW/K}$
  - Heat demand  $285 \text{ kW}$
  - AMTD  $= 285 / 71.7 = 4 \text{ K}$
  - $T_{m,air} = 14.25^\circ\text{C}$
  - $T_{m \text{ water}} = 14.25 + 4 = 18.25^\circ\text{C}.$
- 
- This is almost ridiculously low.
  - The  $\Delta T$  on the liquid side will be  $285/825 * 5 = 1.73 \text{ K}$
  - Meaning that the supply temperature will be  $19.11^\circ\text{C}$  and the return  $17.38^\circ\text{C}$

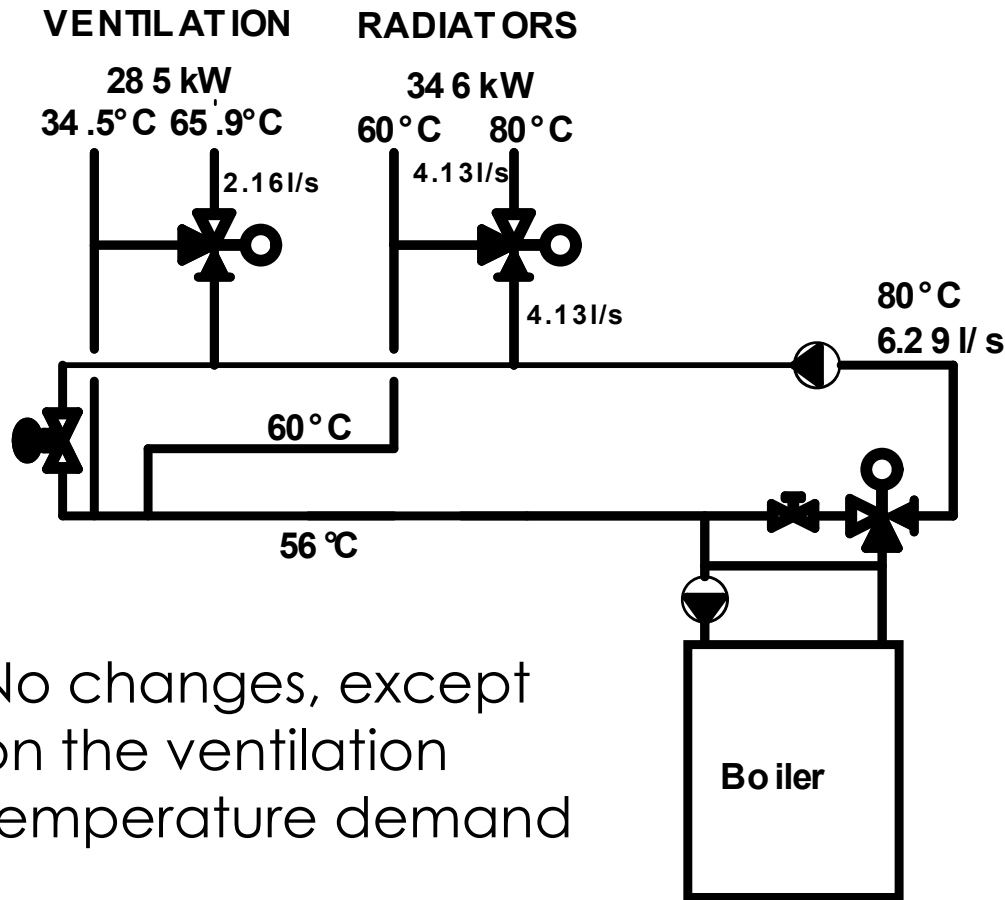
# Cooling coil as a combi-coil

- Flow through the cooling coil :
- $\dot{m} = \frac{\dot{Q}}{c \times \Delta T} = \frac{825}{4.186 \times 5} = 39.4 \frac{kg}{s} \approx 39.4 \frac{l}{s}$
- Flow from header : 2.16 l/s
- A  $\Delta T$  of 1.73 at the coil thereby becomes 31.56 at the header.
- Meaning that the minimum temperature at the header to the coil must be app. 49°C or above.

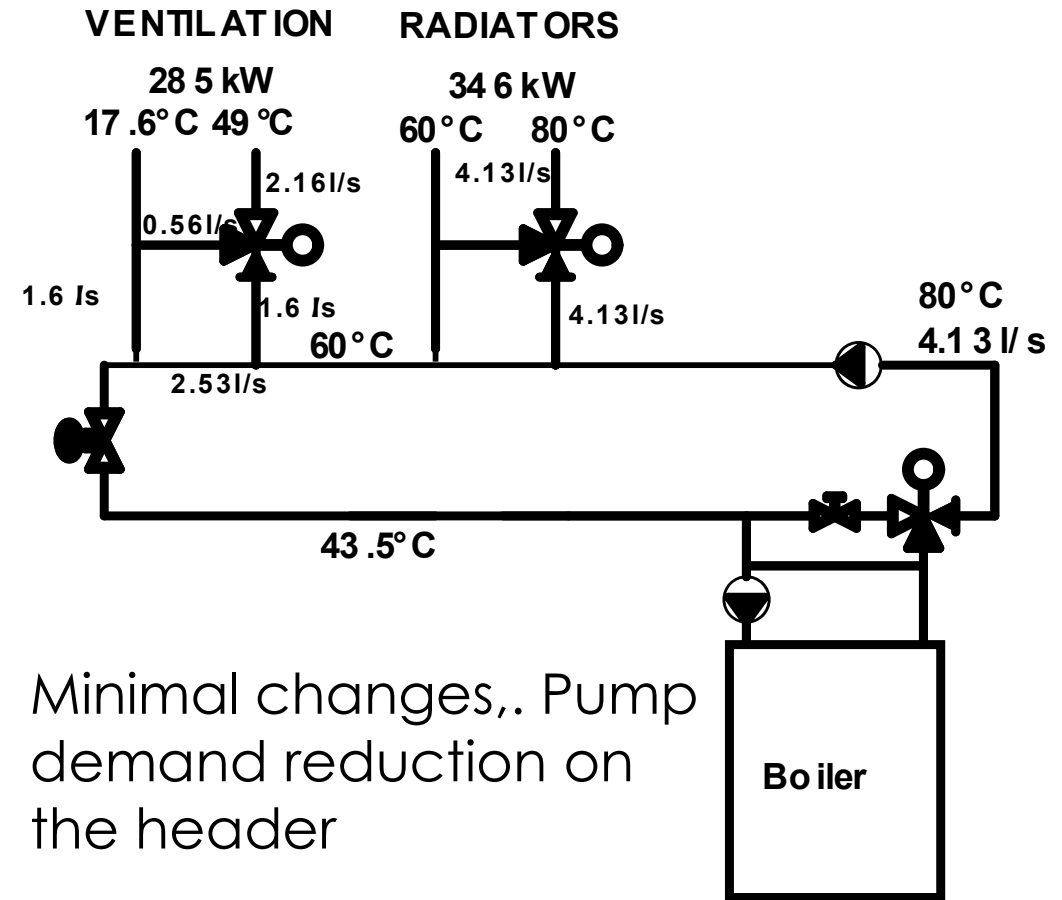
# Why doing all this?

- If we want to implement the use of heat pumps, we have to bring the systems temperatures down.
- Cooling coil as heating coil => low temperature demand.
- No problems with serial connection of radiators and ventilation heat.

# Why doing all this?



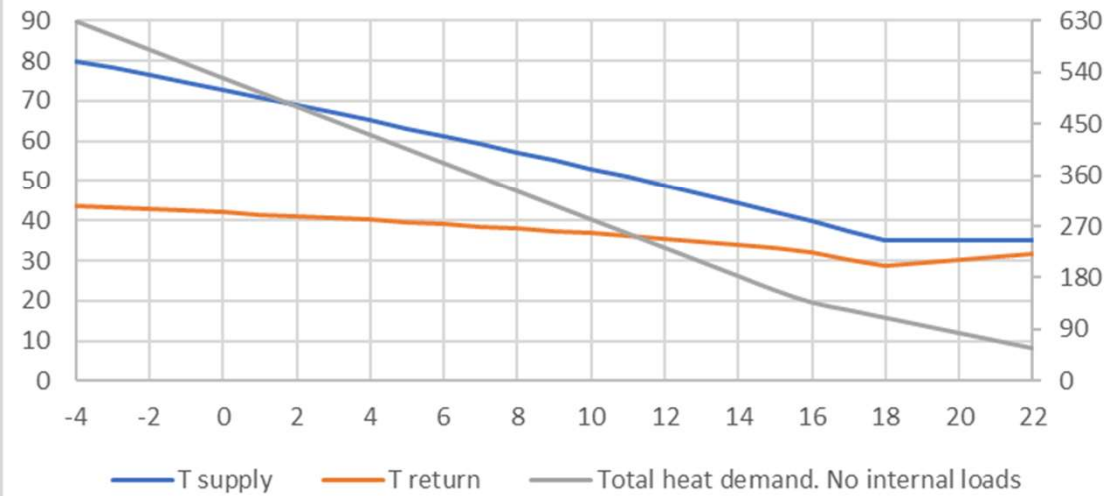
No changes, except on the ventilation temperature demand



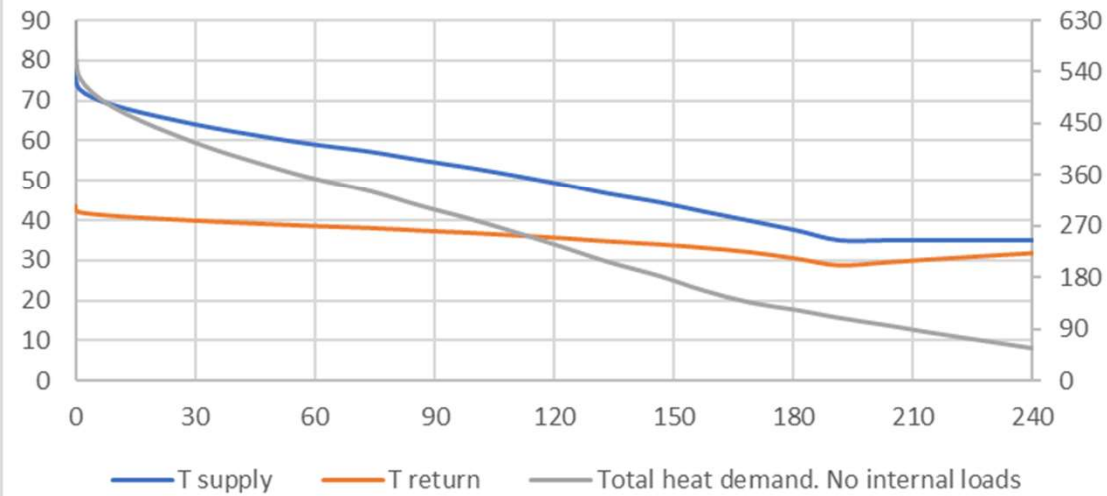
Minimal changes, Pump demand reduction on the header

# Why doing all this?

System temperature demand. Radiators and ventilation in series.



System temperature demand. Radiators and ventilation in series.



# Dwellings

- Basically, dwellings are easier to handle.
- An option always available is the air to air unit.
- The indoor part from my own home.
- When building new or refurbishing, the best option is underfloor heating with heat pump.

